

Table 1. Standard Solutions for Osmometer Calibration*

| Standard Solutions (Weight in g of sodium chloride per kg of water) | Osmolality (mOsmol/kg) (ξ_m) | Molal Osmotic Coefficient ($\Phi_{m,NaCl}$) | Freezing Point Depression (°) ΔT_f |
|---|--|---|--|
| 3.087 | 100 | 0.9463 | 0.186 |
| 6.260 | 200 | 0.9337 | 0.372 |
| 9.463 | 300 | 0.9264 | 0.558 |
| 12.684 | 400 | 0.9215 | 0.744 |
| 15.916 | 500 | 0.9180 | 0.930 |
| 19.147 | 600 | 0.9157 | 1.116 |
| 22.380 | 700 | 0.9140 | 1.302 |

*Adapted from the *European Pharmacopoeia*, 4th Edition, 2002, p. 50.

resistor sensitive to temperature (thermistor), with an appropriate current- or potential-difference measurement device that may be graduated in temperature change or in osmolality; and a means of mixing the sample.

Osmometers that measure the vapor pressures of solutions are less frequently employed. They require a smaller volume of specimen (generally about 5 μ L), but the accuracy and precision of the resulting osmolality determination are comparable to those obtained by the use of osmometers that depend upon the observed freezing points of solutions.

Standard Solutions—Prepare *Standard Solutions* as specified in *Table 1*, as necessary.²

Test Solution—For a solid for injection, constitute with the appropriate diluent as specified in the instructions on the labeling. For solutions, use the sample as is. [NOTE—A solution can be diluted to bring it within the range of measurement of the osmometer, if necessary, but the results must be expressed as that of the diluted solution and must NOT be multiplied by a dilution factor to calculate the osmolality of the original solution, unless otherwise indicated in the monograph. The molal osmotic coefficient is a function of concentration. Therefore, it changes with dilution.]

Procedure—First, calibrate the instrument by the manufacturer's instructions. Confirm the instrument calibration with at least one solution from *Table 1* such that the osmolality of the *Standard Solution* lies within 50 mOsmol/kg of the expected value of the *Test Solution* or the center of the expected range of osmolality of the *Test Solution*. The instrument reading should be within ± 4 mOsmol per kg from the *Standard Solution*. Introduce an appropriate volume of each *Standard Solution* into the measurement cell as in the manufacturer's instructions, and start the cooling system. Usually, the mixing device is programmed to operate at a temperature below the lowest temperature expected from the freezing point depression. The apparatus indicates when the equilibrium is attained. If necessary, calibrate the osmometer, using an appropriate adjustment device such that the reading corresponds to either the osmolality or freezing point depression value of the *Standard Solution* shown in *Table 1*. [NOTE—If the instrument reading indicates the freezing point depression, the osmolality can be derived by using the appropriate formula under *Osmolality*.] Repeat the procedure with each *Test Solution*. Read the osmolality of the *Test Solution* directly, or calculate it from the measured freezing point depression.

Assuming that the value of the osmotic coefficient is essentially the same whether the concentration is expressed in molality or molarity, the experimentally determined osmolality of a solution can be converted to osmolarity in the same manner in which the concentration of a solution is converted from molality to molarity. Unless a solution is very

concentrated, the osmolarity of a solution (ξ_c) can be calculated from its experimentally determined osmolality (ξ_m):

$$\xi_c = 1000\xi_m / (1000 / \rho + \sum w_i v_i)$$

where w_i is the weight in g; and v_i is the partial specific volume, in mL per g, of the i^{th} solute. The partial specific volume of a solute is the change in volume of a solution when an additional 1 g of solute is dissolved in the solution. This volume can be determined by the measurement of densities of the solution before and after the addition of the solute. The partial specific volumes of salts are generally very small, around 0.1 mL per g. However, those of other solutes are generally higher. For example, the partial specific volumes of amino acids are in the range of 0.6–0.9 mL per g. It can be shown from the above equation correlating osmolality with osmolarity that,

$$\xi_c = \xi_m (\rho - c)$$

where ρ is the density of the solution, and c is the total solute concentration, both expressed in g per mL. Thus, alternatively, the osmolarity can also be calculated from experimentally determined osmolality from the measurement of density of the solution by a suitable method and the total weight of the solute, after correction for water content, dissolved per mL of the solution.

(786) PARTICLE SIZE DISTRIBUTION ESTIMATION BY ANALYTICAL SIEVING

Sieving is one of the oldest methods of classifying powders and granules by particle size distribution. When using a woven sieve cloth, the sieving will essentially sort the particles by their intermediate size dimension (i.e., breadth or width). Mechanical sieving is most suitable where the majority of the particles are larger than about 75 μ m. For smaller particles, the light weight provides insufficient force during sieving to overcome the surface forces of cohesion and adhesion that cause the particles to stick to each other and to the sieve, and thus cause particles that would be expected to pass through the sieve to be retained. For such materials, other means of agitation such as air-jet sieving or sonic sifting may be more appropriate. Nevertheless, sieving can sometimes be used for some powders or granules having median particle sizes smaller than 75 μ m where the method can be validated. In pharmaceutical terms, sieving is usually the method of choice for classification of the

²Commercially available solutions for osmometer calibration, with osmolalities equal to or different from those listed in *Table 1* and standardized by methods traceable to NIST, may be used.

coarser grades of single powders or granules. It is a particularly attractive method in that powders and granules are classified only on the basis of particle size, and in most cases the analysis can be carried out in the dry state.

Among the limitations of the sieving method are the need for an appreciable amount of sample (normally at least 25 g, depending on the density of the powder or granule, and the diameter of test sieves) and difficulty in sieving oily or other cohesive powders or granules that tend to clog the sieve openings. The method is essentially a two-dimensional estimate of size because passage through the sieve aperture is frequently more dependent on maximum width and thickness than on length.

This method is intended for estimation of the total particle size distribution of a single material. It is not intended for determination of the proportion of particles passing or retained on one or two sieves.

Estimate the particle size distribution as described under *Dry Sieving Method*, unless otherwise specified in the individual monograph. Where difficulty is experienced in reaching the endpoint (i.e., material does not readily pass through the sieves) or when it is necessary to use the finer end of the sieving range (below 75 μm), serious consideration should be given to the use of an alternative particle-sizing method.

Sieving should be carried out under conditions that do not cause the test sample to gain or lose moisture. The relative humidity of the environment in which the sieving is carried out should be controlled to prevent moisture uptake or loss by the sample. In the absence of evidence to the contrary, analytical test sieving is normally carried out at ambient humidity. Any special conditions that apply to a

particular material should be detailed in the individual monograph.

Principles of Analytical Sieving—Analytical test sieves are constructed from a woven-wire mesh, which is of simple weave that is assumed to give nearly square apertures and is sealed into the base of an open cylindrical container. The basic analytical method involves stacking the sieves on top of one another in ascending degrees of coarseness, and then placing the test powder on the top sieve.

The nest of sieves is subjected to a standardized period of agitation, and then the weight of material retained on each sieve is accurately determined. The test gives the weight percentage of powder in each sieve size range.

This sieving process for estimating the particle size distribution of a single pharmaceutical powder is generally intended for use where at least 80% of the particles are larger than 75 μm. The size parameter involved in determining particle size distribution by analytical sieving is the length of the side of the minimum square aperture through which the particle will pass.

TEST SIEVES

Test sieves suitable for pharmacopeial tests conform to the most current edition of International Organization for Standardization Specification ISO 3310-1: Test Sieves—Technical Requirements and Testing (see *Table 1*). Unless otherwise specified in the monograph, use those ISO sieves listed as principal sizes in *Table 1*. Unless otherwise specified in the monograph, use those ISO sieves listed in *Table 1* as recommended in the particular region.

Table 1. Sizes of Standard Sieve Series in Range of Interest

| ISO Nominal Aperture | | | US Sieve No. | Recommended USP Sieves (microns) | European Sieve No. | Japan Sieve No. |
|----------------------|---------------------|----------|--------------|----------------------------------|--------------------|-----------------|
| Principal Sizes | Supplementary Sizes | | | | | |
| R 20/3 | R 20 | R 40/3 | | | | |
| 11.20 mm | 11.20 mm | 11.20 mm | | | 11200 | |
| | 10.00 mm | | | | | |
| | | 9.50 mm | | | | |
| | 9.00 mm | | | | | |
| 8.00 mm | 8.00 mm | 8.00 mm | | | | |
| | 7.10 mm | | | | | |
| | | 6.70 mm | | | | |
| | 6.30 mm | | | | | |
| 5.60 mm | 5.60 mm | 5.60 mm | | | 5600 | 3.5 |
| | 5.00 mm | | | | | |
| | | 4.75 mm | | | | 4 |
| | 4.50 mm | | | | | |
| 4.00 mm | 4.00 mm | 4.00 mm | 5 | 4000 | 4000 | 4.7 |
| | 3.55 mm | | | | | |
| | | 3.35 mm | 6 | | | 5.5 |
| | 3.15 mm | | | | | |
| 2.80 mm | 2.80 mm | 2.80 mm | 7 | 2800 | 2800 | 6.5 |
| | 2.50 mm | | | | | |
| | | 2.36 mm | 8 | | | 7.5 |
| | 2.24 mm | | | | | |
| 2.00 mm | 2.00 mm | 2.00 mm | 10 | 2000 | 2000 | 8.6 |
| | 1.80 mm | | | | | |
| | | 1.70 mm | 12 | | | 10 |
| | 1.60 mm | | | | | |
| 1.40 mm | 1.40 mm | 1.40 mm | 14 | 1400 | 1400 | 12 |
| | 1.25 mm | | | | | |
| | | 1.18 mm | 16 | | | 14 |
| | 1.12 mm | | | | | |
| 1.00 mm | 1.00 mm | 1.00 mm | 18 | 1000 | 1000 | 16 |
| | 900 μm | | | | | |
| | | 850 μm | 20 | | | 18 |

Table 1. Sizes of Standard Sieve Series in Range of Interest (Continued)

| ISO Nominal Aperture | | | US Sieve No. | Recommended USP Sieves (microns) | European Sieve No. | Japan Sieve No. |
|----------------------|---------------------|--------|--------------|----------------------------------|--------------------|-----------------|
| Principal Sizes | Supplementary Sizes | | | | | |
| R 20/3 | R 20 | R 40/3 | | | | |
| | 800 µm | | | | | |
| 710 µm | 710 µm | 710 µm | 25 | 710 | 710 | 22 |
| | 630 µm | | | | | |
| | | 600 µm | 30 | | | 26 |
| | 560 µm | | | | | |
| 500 µm | 500 µm | 500 µm | 35 | 500 | 500 | 30 |
| | 450 µm | | | | | |
| | | 425 µm | 40 | | | 36 |
| | 400 µm | | | | | |
| 355 µm | 355 µm | 355 µm | 45 | 355 | 355 | 42 |
| | 315 µm | | | | | |
| | | 300 µm | 50 | | | 50 |
| | 280 µm | | | | | |
| 250 µm | 250 µm | 250 µm | 60 | 250 | 250 | 60 |
| | 224 µm | | | | | |
| | | 212 µm | 70 | | | 70 |
| | 200 µm | | | | | |
| 180 µm | 180 µm | 180 µm | 80 | 180 | 180 | 83 |
| | 160 µm | | | | | |
| | | 150 µm | 100 | | | 100 |
| | 140 µm | | | | | |
| 125 µm | 125 µm | 125 µm | 120 | 125 | 125 | 119 |
| | 112 µm | | | | | |
| | | 106 µm | 140 | | | 140 |
| | 100 µm | | | | | |
| 90 µm | 90 µm | 90 µm | 170 | 90 | 90 | 166 |
| | 80 µm | | | | | |
| | | 75 µm | 200 | | | 200 |
| | 71 µm | | | | | |
| 63 µm | 63 µm | 63 µm | 230 | 63 | 63 | 235 |
| | 56 µm | | | | | |
| | | 53 µm | 270 | | | 282 |
| | 50 µm | | | | | |
| 45 µm | 45 µm | 45 µm | 325 | 45 | 45 | 330 |
| | 40 µm | | | | | |
| | | 38 µm | | | 38 | 391 |

Sieves are selected to cover the entire range of particle sizes present in the test specimen. A nest of sieves having a $\sqrt{2}$ progression of the area of the sieve openings is recommended. The nest of sieves is assembled with the coarsest screen at the top and the finest at the bottom. Use micrometers or millimeters in denoting test sieve openings. [NOTE—Mesh numbers are provided in the table for conversion purposes only.] Test sieves are made from stainless steel or, less preferably, from brass or other suitable nonreactive wire.

Calibration and recalibration of test sieves is in accordance with the most current edition of ISO 3310-1. Sieves should be carefully examined for gross distortions and fractures, especially at their screen frame joints, before use. Sieves may be calibrated optically to estimate the average opening size, and opening variability, of the sieve mesh. Alternatively, for the evaluation of the effective opening of test sieves in the size range of 212 to 850 µm, Standard Glass Spheres are available. Unless otherwise specified in the individual monograph, perform the sieve analysis at controlled room temperature and at ambient relative humidity.

Cleaning Test Sieves—Ideally, test sieves should be cleaned using only an air jet or a liquid stream. If some apertures remain blocked by test particles, careful gentle brushing may be used as a last resort.

Test Specimen—If the test specimen weight is not given in the monograph for a particular material, use a test specimen having a weight between 25 and 100 g, depending on

the bulk density of the material, and test sieves having a 200-mm diameter. For 76-mm sieves, the amount of material that can be accommodated is approximately 1/7th that which can be accommodated on a 200-mm sieve. Determine the most appropriate weight for a given material by test sieving accurately weighed specimens of different weights, such as 25, 50, and 100 g, for the same time period on a mechanical shaker. [NOTE—If the test results are similar for the 25-g and 50-g specimens, but the 100-g specimen shows a lower percentage through the finest sieve, the 100-g specimen size is too large.] Where only a specimen of 10 to 25 g is available, smaller diameter test sieves conforming to the same mesh specifications may be substituted, but the endpoint must be redetermined. The use of test samples having a smaller mass (e.g., down to 5 g) may be needed. For materials with low apparent particle density, or for materials mainly comprising particles with a highly isodiametrical shape, specimen weights below 5 g for a 200-mm screen may be necessary to avoid excessive blocking of the sieve. During validation of a particular sieve analysis method, it is expected that the problem of sieve blocking will have been addressed.

If the test material is prone to picking up or losing significant amounts of water with varying humidity, the test must be carried out in an appropriately controlled environment. Similarly, if the test material is known to develop an electrostatic charge, careful observation must be made to ensure

that such charging is not influencing the analysis. An anti-static agent, such as colloidal silicon dioxide and/or aluminum oxide, may be added at a 0.5 percent (m/m) level to minimize this effect. If both of the above effects cannot be eliminated, an alternative particle-sizing technique must be selected.

Agitation Methods—Several different sieve and powder agitation devices are commercially available, all of which may be used to perform sieve analyses. However, the different methods of agitation may give different results for sieve analyses and endpoint determinations because of the different types and magnitude of the forces acting on the individual particles under test. Methods using mechanical agitation or electromagnetic agitation, and that can induce either a vertical oscillation or a horizontal circular motion, or tapping or a combination of both tapping and horizontal circular motion are available. Entrainment of the particles in an air stream may also be used. The results must indicate which agitation method was used and the agitation parameters used (if they can be varied), because changes in the agitation conditions will give different results for the sieve analysis and endpoint determinations, and may be sufficiently different to give a failing result under some circumstances.

Endpoint Determination—The test sieving analysis is complete when the weight on any of the test sieves does not change by more than 5% or 0.1 g (10% in the case of 76-mm sieves) of the previous weight on that sieve. If less than 5% of the total specimen weight is present on a given sieve, the endpoint for that sieve is increased to a weight change of not more than 20% of the previous weight on that sieve.

If more than 50% of the total specimen weight is found on any one sieve, unless this is indicated in the monograph, the test should be repeated, but with the addition to the sieve nest of a more coarse sieve, intermediate between that carrying the excessive weight and the next coarsest sieve in the original nest, i.e., addition of the ISO series sieve omitted from the nest of sieves.

SIEVING METHODS

Mechanical Agitation

Dry Sieving Method—Tare each test sieve to the nearest 0.1 g. Place an accurately weighed quantity of test specimen on the top (coarsest) sieve, and replace the lid. Agitate the nest of sieves for 5 minutes. Then carefully remove each from the nest without loss of material. Reweigh each sieve, and determine the weight of material on each sieve. Determine the weight of material in the collecting pan in a similar manner. Reassemble the nest of sieves, and agitate for 5 minutes. Remove and weigh each sieve as previously described. Repeat these steps until the endpoint criteria are met (see *Endpoint Determination* under *Test Sieves*). Upon completion of the analysis, reconcile the weights of material. Total losses must not exceed 5% of the weight of the original test specimen.

Repeat the analysis with a fresh specimen, but using a single sieving time equal to that of the combined times used above. Confirm that this sieving time conforms to the requirements for endpoint determination. When this endpoint has been validated for a specific material, then a single fixed time of sieving may be used for future analyses, providing the particle size distribution falls within normal variation.

If there is evidence that the particles retained on any sieve are aggregates rather than single particles, the use of mechanical dry sieving is unlikely to give good reproducibility, and a different particle size analysis method should be used.

Air Entrainment Methods

Air Jet and Sonic Sifter Sieving—Different types of commercial equipment that use a moving air current are available for sieving. A system that uses a single sieve at a time is referred to as air jet sieving. It uses the same general sieving methodology as that described under the *Dry Sieving Method*, but with a standardized air jet replacing the normal agitation mechanism. It requires sequential analyses on individual sieves starting with the finest sieve to obtain a particle size distribution. Air jet sieving often includes the use of finer test sieves than those used in ordinary dry sieving. This technique is more suitable where only oversize or undersize fractions are needed.

In the sonic sifting method, a nest of sieves is used, and the test specimen is carried in a vertically oscillating column of air that lifts the specimen and then carries it back against the mesh openings at a given number of pulses per minute. It may be necessary to lower the sample amount to 5 g, when sonic sifting is employed.

The air jet sieving and sonic sieving methods may be useful for powders or granules when mechanical sieving techniques are incapable of giving a meaningful analysis.

These methods are highly dependent upon proper dispersion of the powder in the air current. This requirement may be hard to achieve if the method is used at the lower end of the sieving range (i.e., below 75 μm), when the particles tend to be more cohesive, and especially if there is any tendency for the material to develop an electrostatic charge. For the above reasons endpoint determination is particularly critical, and it is very important to confirm that the oversize material comprises single particles and is not composed of aggregates.

INTERPRETATION

The raw data must include the weight of test specimen, the total sieving time, and the precise sieving methodology and the set values for any variable parameters, in addition to the weights retained on the individual sieves and in the pan. It may be convenient to convert the raw data into a cumulative weight distribution, and if it is desired to express the distribution in terms of a cumulative weight undersize, the range of sieves used should include a sieve through which all the material passes. If there is evidence on any of the test sieves that the material remaining on it is composed of aggregates formed during the sieving process, the analysis is invalid.

<788> PARTICULATE MATTER IN INJECTIONS

This general chapter is harmonized with the corresponding texts of the *European Pharmacopoeia* and/or the *Japanese Pharmacopoeia*. These pharmacopoeias have undertaken not to make any unilateral change to this harmonized chapter. Portions of the present general chapter text that are national USP text, and therefore not part of the harmonized text, are marked with symbols (\star) to specify this fact.

Particulate matter in injections and parenteral infusions consists of extraneous mobile undissolved particles, other than gas bubbles, unintentionally present in the solutions. \star As stated in *Injections* <1>, solutions for injection administered by the intramuscular or subcutaneous route must meet the requirements of *Particulate Matter in Injections* <788>. Parenterals packaged and labeled exclusively for use